## OPERATION

\&

## SERVICE MANUAL

## SMA5005 \& SMA5015

H Bridge Linear Servo Drives


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## INTRODUCTION

The Glentek SMA5005 and SMA5015 H bridge Linear Servo Drives provide the optimum solution for applications which require high current loop bandwidth, low radiated electrical noise, and low crossover distortion. The SMA5015 Drive incorporates our latest generation ISO-BIAS current sense technology, which provides one of the lowest drift linear Drives on the market today. These Drives are constructed using surface mount technology and incorporate the latest in heat transfer technology which make them one of the most powerful Drives for a given form factor.

Typical applications are brushed DC permanent magnet motors and voice coil motors.
The SMA5005 \& SMA5015 are configurable and can operate in the following modes:

1. Velocity mode for motors with tachometer feedback*
2. Current mode for torque mode operation
*High performance models only support current mode
A basic velocity mode servo loop for a brush type motor is shown in figure A. An external controller commands a given velocity (RPM). The velocity loop summing Drive compares this command with the actual motor velocity, supplied by a DC tachometer on the motor shaft, and produces an error voltage proportional to the difference between the actual and commanded velocity.

The velocity error is used to command motor current in the inner servo-loop. The current loop summing Drive compares the command current (velocity error) with the actual current in the motor and produces an error voltage proportional to the difference between the actual and commanded current.

Finally, the current error signal is used to produce an output to drive the motor.
The velocity loop may be bypassed, and an external current command fed directly to the current loop. In this case, the external command signal controls the torque of the motor, rather than the velocity. This is known as current-mode operation.


Figure A - Velocity mode servo loop for a brush type motor

## FEATURES

| - Ergonomic Design | Easy access to connections, adjustments and test points. |
| :--- | :--- |
| - SMT construction | Provides ultra compact size, cost competitive package and high <br> reliability. |
|  | Standard performance models have a nominal 10 kHz current loop <br> bandwidth which varies with the motor inductance. <br> - Bandwidth <br> current loop bandwidth which varies with the motor inductance. |
|  | Provides high bandwidth, low noise and zero crossover distortion. |
| - Linear output stage | Velocity mode (tachometer feedback), Current mode (torque) and <br> - Multimode operation |
|  | Operating input voltage range 17-0-17 to 39-0-39 VAC for standard |
| - Operating Voltage | SMA5015 stand alone (higher voltages available) 24-75 VDC for <br> standard SMA5005 module. |
| Velocity and current modes (SMA5015 is field configurable). |  |

## APPLICATION NOTE

## POWER DISSIPATION CONSIDERATIONS AND CALCULATIONS WHEN USING LINEAR DC SERVO DRIVES:

When selecting a linear Drive, the following ratings of the Drive should be known in order to properly size the Drive to your system requirements:

1- The total wattage, peak current, and voltage rating of all the semiconductors installed on the heat sink of the output power stage of the Drive.

Output transistor ratings for the SMA5005 series are:
Voltage: 250 Volts
Peak current: 60 A; Continuous current: 30 A (Normally shipped with 12-20A limit)
Total wattage @25 deg C.: 1200 Watts
Output transistor ratings for the SMA5015 series are:
Voltage: 200 Volts
Peak current: 240 A; Continuous current: 60 A (Normally shipped with 20-50A limit)
Total wattage @25 deg C.:4480 Watts
The SMA5005 series Drive is a module requiring an external unregulated single polarity DC power supply. Glentek offers various unregulated power supplies for the SMA5005 series Drives.

The SMA5005 series Drive is also available in multi-axis configurations. That is, there are two basic baseplate assemblies namely 2 -axis and 4 -axis baseplate assemblies that have built-in AC to DC power supplies (un-regulated) and cooling fans. The 2 -axis baseplate assembly contains one AC to DC power supply, one fan, and up to two SMA5005 Drive modules. The 4-axis baseplate assembly contains one AC to DC power supply, two fans, and up to four SMA5005 Drive modules. For multi-axis applications, it is always recommended to use three phases power transformers for minimizing ripple voltage during high current demand scenarios where all axis motors are running at full load simultaneously. Glentek offers various isolated three phases power transformers.

The SMA5015 series is a stand-alone style Drive, meaning that the unregulated dual polarity power supply is mounted within the Drive enclosure. Glentek offers 1.4 KVA and 2.0KVA center tapped power transformers for the SMA5015 series Drives.

2- Typical continuous internal power dissipation rating of the Drives running at normal room conditions is:

SMA5005-xLB series (L-bracket heatsink); 100 Watts continuous
SMA5005-xSF series (short fin heatsink); 250 Watts continuous
SMA5015 series; 300 Watts continuous
For most applications, the above heat sinking is adequate. However, if you have a usage mode where the heat sink temperature becomes excessive, please contact Glentek and we can furnish a larger heat sink with greater air flow for your application.

Use the following relationships to calculate Drive dissipation:

1) $\mathbf{P d}=\operatorname{Im} x \mathrm{Vb}$ (watts)

Where: $\mathrm{Pd}=$ Total watts delivered from bus
$\mathrm{Im}=$ Motor current
$\mathrm{Vb}=$ Bus voltage
2) $\mathbf{P m}=\operatorname{Im} x$ Vm (watts)

Where: $\mathrm{Pm}=$ Total power (watts) dissipated in motor
$\mathrm{Vm}=$ Motor voltage
3) $\mathbf{P a}=\operatorname{lm} \times \mathbf{V b}-\operatorname{lm} \times \mathrm{Vm}$

Where: $\mathrm{Pa}=$ Total watts dissipated at Drive
From the above relationship, it can be surmised that the worst case dissipation occurs when the Drive has to deliver a high continuous current at a low motor speed, i.e., less motor BEMF and more current. For some applications, a power resistor can be added in series with the motor thus shifting some of the power dissipation from the Drive to the resistor.

## TECHNICAL SPECIFICATIONS

## Output

- SMA5005: 15A peak, 5A continuous, (forced air cooling required)

Note: Large motor and small motor versions have different velocity loop compensation.

- SMA5015: 25A peak, 10A continuous, (integral fan cooling)


## Rated Internal Power Dissipation

- SMA5005-xLB series (L-bracket heatsink); 100 Watts continuous
- SMA5005-xSF series (short fin heatsink); 250 Watts continuous
- SMA5015 series; 300 Watts continuous


## Input

- SMA5005: 24-75VDC
- SMA5015: 17-0-17VAC to 39-0-39VAC (+/-24 to +/-55VDC Bipolar Input)
- Integral forced air fan cooling (multi-axis SMA5005 and SMA5015 only)
- Analog command signals: differential \& single ended, adjustable gain
- Manual reset Pushbutton switch (SMA5015 only)
- Reset: SMA5005: pull up/pull down, active high, active low

SMA5015: pull up/pull down, active high, active low

- Inhibit: Same as Reset
- +/- Limits: Same as Reset

Refer to Drive Configuration Code on page 11 for more information on signals input options

## Output Connections

- Motor: MTR + \& MTR-
- Fault out: SMA5005: Optically isolated can sink up to 50 mA , active high only

SMA5015: Open collector, Pulled Up (+5V), active high or active low

## Bandwidth

- 10 kHz maximum and varies with motor inductance for standard performance models
- 15 kHz maximum and varies with motor inductance for high performance models


## Status Indicator

- SMA5005: Green Run LED, Red Inhibit LED, Red Fault LED
- SMA5015: 7-segment LED display indicates Drive status and diagnostics


## Mechanical

- SMA5005-xLB module: Height: 4.87", Width: 1.20", Depth: 7.13"
- SMA5005-xSF module: Height: 4.87", Width: 1.88", Depth: 7.13"
- SMA5005 2-Axis: Height: 6.93", Width: 9.75 ", Depth: 10.75 "
- SMA5005 4-Axis: Height: 6.93", Width: 14.88", Depth: 10.75"
- SMA5015 stand-alone: Height: 9.00", Width: 4.25", Depth: 14.50"


## Environmental

- Operating temperature 0 to $55^{\circ} \mathrm{C}$
- Storage temperature -40 to $80^{\circ} \mathrm{C}$
- Humidity $5-95 \%$ relative (non-condensing)


## MODEL NUMBERING

The information below should be used to order your Drive pre-configured for your application. You may wish to have a Glentek application engineer confirm your configuration because field configuration options are limited.

## Standard Performance Drive Model Numbering:

SMA5005—xx—bbb—1

## Drive Model Number <br> $\qquad$

Velocity Loop Compensation
Leave blank for standard performance current mode drives
S = Small Motor (less than 3 " in diameter)
$\mathbf{L}=$ Large Motor ( $3^{\prime \prime}$ or greater in diameter)

Single Module
Drive Configuration Code
See configuration algorithm on page 11
Internal Heat Dissipation
LB = 100 W (L-bracket heatsink) SF =250 W (Short fin heatsink)

SMA5005—xx—bbb-eA-g
Drive Model Number
Velocity Loop Compensation
Leave blank for standard performance current mode drives
$\mathbf{S}=$ Small Motor (less than 3 " in diameter)
$\mathrm{L}=$ Large Motor (3" or greater in diameter)
Internal Heat Dissipation
LB = 100 W (L-bracket heatsink) SF =250 W (Short fin heatsink)


Standard performance servo drives have a nominal 10 kHz current loop bandwidth which varies with the motor inductance.

High Performance Drive Model Numbering:


## SMA5005-4x-34C-eA-g



High performance servo drives have a nominal 15 kHz current loop bandwidth which varies with the motor inductance.

Standalone model only available as a standard performance servo drive
Note that high performance models have 34C fixed configuration code.
Reset is pulled down active high, inhibit is pulled up active high, and there are no +/- limits. Signal input is set for differential, but can be configured for single ended input by externally grounding one of the two signal input lines.

Due to the high performance and high current loop bandwidth, voice coil/motor parameters, operating voltage, and desired current loop bandwidth are required upon ordering.

| Inhibit, Reset, $\pm$ Limit Configuration |  |  |  |
| :---: | :---: | :---: | :---: |
| Type | Input is: | Input State: | Binary Code |
| A | Internally Pulled Up | Active When Low | 00 |
| C | Internally Pulled Up | Active When High | 01 |
| D | Internally Pulled Down | Active When Low | 10 |
| B | Internally Pulled Down | Active When High | 11 |


| Logic Input Configuration for Inhibit |  |
| :--- | :--- |
| Type A | Requires grounding of input to disable the Drive. |
| Type B | Requires a positive voltage at input to disable the Drive. |
| Type C | Requires grounding of input to enable the Drive. |
| Type D | Requires a positive voltage at input to enable the Drive. |


| Important Notes: |
| :---: |
| SMA5005 is not field configurable <br> except signal input |
| SMA5015 logic inputs are hard <br> wired, either pulled up or <br> pulled down at the factory |
| High performance SMA5005 has <br> configuration code 34C: |
| Reset is Pulled down, Active high <br> Inhibit is Pulled up, Active high <br> $\pm L i m i t ~ i s ~ P u l l e d ~ u p, ~ A c t i v e ~ h i g h ~$ |
| Differential input |
| Current mode |
| +15 V Input logic pull up voltage select |

## Drive Configuration Code



## START UP AND CALIBRATION

This section contains the procedure required for initial start up and Drive calibration. The standard performance SMA5005 and SMA5015 series Drives can be configured to run in velocity mode and current mode. The high performance SMA5005 Drives can only run in current mode.

Required Equipment: Oscilloscope, voltmeter \& battery box. The battery box serves as a step input voltage command, applying and removing a flashlight battery can also be used for this function. Glentek sells a battery box BB-700 which is ideal for this function.

Refer to the technical specifications page and the drawings in the appendix for the information needed to supply the correct power and to wire the model you are starting up. An isolation transformer is needed for the multi-axis SMA5005 and SMA5015. An isolated power supply (unregulated is OK) providing the necessary voltage is required for the SMA5005 module. Glentek can provide appropriate transformers and power supplies. Consult a Glentek applications engineer or sales person for assistance.

## A. Initial Start Up

When applying power to start up your Drive system for the first time, we recommend you follow this procedure. If you have already gone through this procedure, you can skip to the appropriate calibration procedure.

1. Check for any loose or damaged components.
2. Check that all connections are tight.
3. Be sure that the motor mechanism is clear of obstructions. If the mechanism has limited motion, e.g. a lead-screw, set the mechanism to mid-position.
4. Disconnect the signal and auxiliary inputs.
5. Be sure the Loop-Gain pot(s) are fully CCW (RV7 for SMA5005, and RV4 for SMA5015). This will prevent the motor from running away in velocity mode when power is applied.
6. Check for the correct AC voltage before connecting to SMA5005 multi-axis or SMA5015 Drives. The DC Bus (Drive supply-voltage) will be 1.4 times greater than the AC value. If the voltage is correct, remove power and connect AC source to Drive inputs. For SMA5005 module Drive, check for the correct DC voltage before connecting to the Drive power input.
7. Work on only one Drive axis at a time for SMA5005 multi-axis Drives.

## B. Calibration of the Velocity Mode of a Standard Performance Drive (SMA5005 Series)

The Drive, in this configuration, receives an analog, bi-polar input command, which is proportional to the motor velocity. The Drive receives velocity feedback from a tachometer, which is usually mounted to the rear of the motor. The following pots will be set during calibration: (Note: RV7 is a single turn pot and RV1-RV5 are 20-turn pots.)

| Pots | Name of Pot | Notes |
| :---: | :---: | :--- |
| RV1 | Signal Gain, SIG | Sets the input voltage to velocity ratio. |
| RV2 | Balance, BAL | Used to null any offset in the system. |
| RV3 | Compensation, COMP | Used in conjunction with Tach. Gain to set the system <br> bandwidth. |
| RV4 | Tach. Gain, TACH | Sets the DC tachometer gain. |
| RV5 | Current Limit, I LIMIT | Sets the maximum motor current. Shipped set CW (max). |
| RV7 | Loop Gain, <br> LOOP GAIN | Used to shut off uncalibrated Drives. When the loop gain is fully <br> CCW, no current is delivered to the motor. |

PROCEDURE:

1. Connect motor cables to DC Input/Motor Output pin 4 (MOTOR+) and DC Input/Motor Output pin 5 (MOTOR-). Connect the motor ground to the chassis ground (or PE).
2. Connect the Tach. wires to Controller I/O pin 3 (TACH IN-) and Controller I/O pin 4 (TACH IN+ 'GND').
3. Apply main power and fan power. Visually confirm a green LED. Depending on the configuration of the Inhibit, Reset and +/-Limits, it may be necessary to make appropriate connections to those terminals before the Drive will be enabled and energize the motor.
4. Slowly turn the Loop Gain (RV7) CW fully. Motor should be stopped or turning slowly. If the motor starts running away, remove the power, reverse the Tach. leads, and apply power.
5. Set Balance (RV2) for zero motor rotation.
6. Connect oscilloscope probe to Controller I/O pin 7 (CURRENT SENSE) and oscilloscope ground to Controller I/O pin 13, 14 or 15 (SIGNAL GND). Connect battery box to Controller I/O pin 1 (SIGNAL+) and Controller I/O pin 2 (SIGNAL-). The voltage on Controller I/O pin 7 is a function of motor current: $1 \mathrm{~V}=2.0 \mathrm{~A}$. While applying a step input voltage, adjust the Current Limit (RV5) for desired peak current.
7. The purpose of the following procedure is to set the system bandwidth to obtain a criticallydamped response (see figure B) or a one hook overshoot response with the maximum possible Tach. Gain. There are many possible settings of Tach. Gain and Compensation which will yield the desired waveform: The optimum setting will occur when Tach. Gain is as CW as possible and Compensation is as CCW as needed. However, the velocity loop may become unstable (the motor oscillates or hums) as the Compensation is tuned CCW (increasing the BW). In this case, stability is the limiting factor: At no time should the velocity loop be allowed to be unstable. Drives are normally shipped with the Tach. Gain (RV4) set at $100 \%$. This is a good place to start. If you are unsure of where the Tach. Gain is set, turn the Tach. Gain (RV4) fully CW (up to 20 turns).
8. Connect oscilloscope probe to Controller I/O pin 3 (TACH IN-) and oscilloscope ground to Controller I/O pin 13, 14 or 15 . Set battery box for a DC signal output to obtain approximately 400RPM. The RPM may be set by measuring the Tach. voltage at Controller I/O pin 3, e.g., 2.8 VDC for a $7 \mathrm{~V} / \mathrm{KRPM}$ Tach. is 400RPM.
9. Pulse the input and compare the waveform with figure B.

A.) Critically Damped Signal

C.) Under Damped Signal

B.) 1 Hook Overshoot Signal

D.) Over Damped Signal

Figure B - Critically damped, One Hook Overshoot, Under and Over damped waveforms
10. Adjust the Compensation pot (RV3) CCW until the waveform is critically damped or one hook overshoot. If the desired waveform cannot be obtained by adjusting the Compensation pot before the motor becomes unstable, back off the Tach. Gain pot (CCW) a few turns.
11. Do not adjust the Tach. Gain or Compensation for the rest of the calibration procedure.
12. Set battery box for a known DC voltage (+/-10V). Adjust the Signal Gain pot (RV1) and set the ratio based on the desired motor velocity.
13. Calibration complete.
14. Now connect the computer control (CNC). If the motor is rotating in the wrong direction for a given input polarity, power down. Reverse both the motor and Tach. leads.

## C. Calibration of the Current Mode of a Standard Performance Drive (SMA5005 Series)

The Drive in this configuration receives an analog, bi-polar input command, which is proportional to the required motor current (motor torque). The following potentiometers (pots) will be set during calibration: (Note: RV7 is a single turn pot and RV1-RV5 are 20-turn pots.)

| Pots | Name of Pot | Notes |
| :---: | :---: | :--- |
| RV1 | Signal Gain, SIG | Sets the input voltage to current ratio. |
| RV2 | Balance, BAL | Used to null any offset in the system. |
| RV3 | Compensation, COMP | Used in conjunction with Tach. Gain to set the system <br> bandwidth. |
| RV4 | Tach. Gain, TACH | Sets the DC tachometer gain. |
| RV5 | Current Limit, I LIMIT | Sets the maximum motor current. Shipped set CW (max). |
| RV7 | Loop Gain, <br> LOOP GAIN | Used to shut off uncalibrated Drives. When the loop gain is <br> fully CCW, no current is delivered to the motor. |

## PROCEDURE:

1. Apply main power and fan power. Visually confirm a green LED. Depending on the configuration of the Inhibit, Reset and +/-Limits, it may be necessary to make appropriate connections to those terminals before the Drive will be enabled and energize the motor.
2. Slowly turn the Loop Gain (RV7) pot CW fully. The Motor should be stopped or turning slowly. Set the Balance (RV2) for OV across DC Input/Motor Output pin 4 to DC Input/Motor Output pin 5.
3. Connect oscilloscope probe to Controller I/O pin 7 (CURRENT SENSE) and oscilloscope ground to Controller I/O pin 13, 14 or 15 (SIGNAL GND). Connect battery box to Controller I/O pin 1 (SIGNAL+) and Controller I/O pin 2 (SIGNAL-). The voltage on Controller I/O pin 7 is a function of motor current: $1 \mathrm{~V}=2.0 \mathrm{~A}$.
4. To set the current limit at some value less than the maximum, apply a large step command and observe peak above desired peak current. Turn current limit pot CCW until peak current is reduced to desired value.
5. Apply a step command of $3-4$ volts. Observe commanded motor (scale is $10 \mathrm{~A} / \mathrm{V}$ ) and set the desired signal to current ratio. For example, 3A/V.
6. If the motor is rotating in the wrong direction for a given input polarity, power down and reverse the motor leads.
7. Calibration complete.

## D. Calibration of the Current Mode of a High Performance Drive (SMA5005-4 Series)

The Drive in this configuration receives an analog, bi-polar input command, which is proportional to the required motor current (motor torque). The following potentiometer (pot) will be set during calibration: (Note: Balance Pot is a 20 -turn pot.)

| Name of Pot | Notes |
| :---: | :--- |
| BALANCE POT | Used to null any offset in the system. |

Calibration is minimal compared to standard performance Drives. The Drive will be custom tuned at the factory for the specific application. Therefore, voice coil/motor parameters, operating voltage, and desired current loop bandwidth are required upon ordering. The only user tunable parameter is balance/current offset.

## PROCEDURE:

1. Apply main power and fan power. Visually confirm a green LED. Depending on the configuration of the Inhibit and Reset pins, it may be necessary to make appropriate connections to those terminals before the Drive will be enabled and energize the motor.
2. The Motor should be stopped or turning slowly. Set the Balance Pot for OV across DC Input/Motor Output pin 4 to DC Input/Motor Output pin 5.
3. If the motor is rotating in the wrong direction for a given input polarity, power down and reverse the motor leads.
4. Calibration complete.

## E. Calibration Setup Record (SMA5005 Series)

It is good practice to keep a record of all the pot settings. Doing so will facilitate calibration on future units and repair on this unit. Although not a substitute for the calibration procedure, it will at least get you "in the ballpark." Remove the power and allow all capacitors to discharge before taking measurements.
Note: The balance pot should not be measured in this fashion, set per step 3 in the calibration procedure.

| Pot/Dip-Switches | AMP1 | AMP2 | AMP3 | AMP4 |
| :--- | :--- | :--- | :--- | :--- |
| Signal Gain pot wiper <br> TP2 to common (ohms): |  |  |  |  |
| Tach. Gain pot wiper <br> TP3 to common (ohms): |  |  |  |  |
| Compensation pot wiper <br> TP4 to common (ohms): |  |  |  |  |
| Current Limit pot wiper <br> TP5 to common (ohms): |  |  |  |  |

Note: Tach. voltage is measured at Controller I/O pin 3. Common for all measurements is at Controller I/O pin 4.

Date data taken: / /
Serial number $\mathrm{S} / \mathrm{N}$ :
Model number:
SMA5005 $\qquad$
Note any changes to components or any special features in the space below:

## F. Calibration of the Velocity Mode Drive (SMA5015 Series)

The Drive, in this configuration, receives an analog, bi-polar input command, which is proportional to the motor velocity. The Drive receives velocity feedback from a tachometer, which is usually mounted to the rear of the motor. The following pots will be set during calibration: (Note: RV7 is a single turn pot and RV1-RV6, RV8-RV10 are 20-turn pots.)
Note: RV9 and RV10 are factory set and should not be adjusted. Adjusting these pots voids warranty.

| Pots | Name of Pot | Notes |
| :---: | :---: | :--- |
| RV1 | Differential Gain, AUX | Sets the input voltage to velocity ratio for differential signal input. |
| RV2 | Signal Gain, SIG | Sets the input voltage to velocity ratio for single-ended signal <br> input. |
| RV3 | Balance, BAL | Used to null any offset in the system. |
| RV4 | Tach. Gain, TACH | Sets the DC tachometer gain. |
| RV5 | Compensation, COMP | Used in conjunction with Tach. Gain to set the system bandwidth. |
| RV6 | Current Limit, I LIMIT | Sets the maximum motor current. Shipped set CW (max). |
| RV7 | Loop Gain, <br> LOOP GAIN | Used to shut off uncalibrated Drives. When the loop gain is fully <br> CCW, no current is delivered to the motor. |

## PROCEDURE:

1. Connect motor cables to TB1 MTR+ and MTR-. Connect the motor ground to chassis ground.
2. Connect the Tach. wires to $\mathrm{J} 1-5$ (TACH. INPUT) and J1-11 (COMMON).
3. Apply main power and fan power. Visually confirm an "O" on the 7 -segment display. Depending on the configuration of the Inhibit, Reset and +/-Limits, it may be necessary to make appropriate connections to those terminals before the Drive will be enabled and energize the motor.
4. Slowly turn the Loop Gain (RV7) CW. Motor should be stopped or turning slowly. If the motor starts running away, remove the power, reverse the Tach. leads, and apply power.
5. Set Balance (RV3) for zero motor rotation.
6. Set the desired peak current limit by adjusting RV6 while measuring voltage at TP6. The ratio is $1 \mathrm{~V}=6 \mathrm{~A}$.
7. The purpose of the following procedure is to set the system bandwidth to obtain a criticallydamped response (see figure C) or a one hook overshoot response with the maximum possible Tach. Gain. There are many possible settings of Tach. Gain and Compensation which will yield the desired waveform: The optimum setting will occur when Tach. Gain is as CW as possible and Compensation is as CCW as needed. However, the velocity loop may become unstable (the motor oscillates or hums) as the Compensation is tuned CCW (increasing the BW). In this case, stability is the limiting factor: At no time should the velocity loop be allowed to be unstable. Drives are normally shipped with the Tach. Gain (RV4) set at $100 \%$. This is a good place to start. If you are unsure of where the Tach. Gain is set, turn the Tach. Gain (RV4) fully CW (up to 20 turns).
8. Connect oscilloscope probe to $\mathrm{J} 1-5$ (TACH INPUT) and oscilloscope ground to $\mathrm{J} 1-11$ (COMMON). Set battery box for a DC signal output to obtain approximately 400RPM. The RPM may be set by measuring the Tach. voltage at $\mathrm{J} 1-5$, e.g., 2.8 VDC for a $7 \mathrm{~V} / \mathrm{KRPM}$ Tach. is 400RPM.
9. Pulse the input and compare the waveform with figure C .


Figure C - Critically damped, One Hook Overshoot, Under and Over damped waveforms
10. Adjust the Compensation pot (RV5) CCW until the waveform is critically damped or one hook overshoot. If the desired waveform cannot be obtained by adjusting the Compensation pot before the motor becomes unstable, back off the Tach. Gain pot (CCW) a few turns.
11. Do not adjust the Tach. Gain or Compensation for the rest of the calibration procedure.
12. Set battery box for a known DC voltage (+/-10V). Adjust the AUX. Gain (RV1) pot for differential Gain or SIG. Gain (RV2) for single-ended input to set the ratio based on the desired motor velocity.
13. Calibration complete.
14. Now connect the computer control (CNC). If the motor is rotating in the wrong direction for a given input polarity, power down. Reverse both the motor and Tach. leads.

## G. Calibration of the Current Mode Drive (SMA5015 Series)

The Drive in this configuration receives an analog, bi-polar input command, which is proportional to the required motor current (motor torque). The following potentiometers (pots) will be set during calibration: (Note: RV7 is a single turn pot and RV1-RV6, RV8-RV10 are 20-turn pots.)

| Pots | Name of Pot | Notes |
| :---: | :---: | :--- |
| RV1 | Differential Gain, AUX | Sets the input voltage to current ratio for differential signal <br> input. |
| RV2 | Signal Gain, SIG | Sets the input voltage to current ratio for single-ended signal <br> input. |
| RV3 | Balance, BAL | Used to null any offset in the system. |
| RV4 | Tach. Gain, TACH | Sets the DC tachometer gain. |
| RV5 | Compensation, COMP | Used in conjunction with Tach. Gain to set the system <br> bandwidth. |
| RV6 | Current Limit, I LIMIT | Sets the maximum motor current. Shipped set CW (max). |
| RV7 | Loop Gain, <br> LOOP GAIN | Used to shut off uncalibrated Drives. When the loop gain is <br> fully CCW, no current is delivered to the motor. |

## PROCEDURE:

1. Apply the main power and fan power. Visually confirm an "O" on the display. Depending on the configuration of the Inhibit, Reset and +/-Limits, it may be necessary to make appropriate connections to those terminals before the Drive will be enabled and energize the motor.
2. Slowly turn the Loop Gain (RV7) pot CW. The Motor should be stopped or turning slowly. Set the Balance (RV3) for OV across TB1 MTR.+ to TB1 MTR.--
3. Set the desired peak current limit by adjusting RV6 while measuring voltage at TP6. The ratio is $1 \mathrm{~V}=6 \mathrm{~A}$. Battery box does not have to be connected to the Drive.
4. If AUX. Gain is desired, monitor voltage across $\mathrm{J} 1-1$ (AUX. INPUT) to J1-2 (AUX. RETURN). If SIG. Gain is desired, monitor voltage across J1-3 (SIG. INPUT) to J1-4 (SIG. COM.). To set the desired signal to current ratio for AUX. Gain adjust the RV1 (differential signal) pot and for SIG. Gain adjust the RV2 (single-ended signal) pot. Apply a step command of 3-4 volts. Observe commanded motor (scale is $10 \mathrm{~A} / \mathrm{V}$ ) and set the desired signal to current ratio. For example, $3 \mathrm{~A} / \mathrm{V}$ (max is $30 \mathrm{~A} / 10 \mathrm{~V}$ ).
5. If the motor is rotating in the wrong direction for a given input polarity, power down and reverse the motor leads.
6. Calibration complete.

## H. Calibration Setup Record (SMA5015 Series)

It is good practice to keep a record of all the pot settings. Doing so will facilitate calibration on future units and repair on this unit. Although not a substitute for the calibration procedure, it will at least get you "in the ballpark." Remove the power and allow all capacitors to discharge before taking measurements. Note: The balance pot should not be measured in this fashion, set per step 3 in the calibration procedure.

| Pot/Dip-Switches | Drive |
| :--- | :--- |
| Differential Gain pot wiper <br> TP1 to common (ohms): |  |
| Signal Gain pot wiper <br> TP2 to common (ohms): |  |
| Tach. Gain pot wiper <br> TP4 to common (ohms): |  |
| Compensation pot wiper <br> TP5 to common (ohms): |  |
| Current Limit pot wiper <br> TP6 to common (ohms): |  |

Note: Tach. voltage is measured at $\mathrm{J} 1-5$. Common for all measurements is at $\mathrm{J} 1-4$.
Date data taken: / /
Serial number $\mathrm{S} / \mathrm{N}$ :
Model number: SMA5015
Note any changes to components or any special features in the space below:

## APPENDIX

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# European Union EMC Directives: Electromagnetic Compatibility Guidelines 

For Machine Design

This document provides background information about Electromagnetic Interference (EMI) and machine design guidelines for Electromagnetic Compatibility (EMC).

## Introduction

Perhaps no other subject related to the installation of industrial electronic equipment is so misunderstood as electrical noise. The subject is complex and the theory easily fills a book. This section provides guidelines that can minimize noise problems.

The majority of installations do not exhibit noise problems. However, these filtering and shielding guidelines are provided as counter measures. The grounding guidelines provided below are simply good grounding practices. They should be followed in all installations.

Electrical noise has two characteristics: generation or emission of electromagnetic interference (EMI) and response or immunity to EMI. The degree to which a device does not emit EMI, and is immune to EMI is called the device's Electromagnetic Compatibility (EMC).

Equipment, which is to be brought into the European Union legally, requires a specific level of EMC. Since this applies when the equipment is brought into use, it is of considerable importance that a drive system, as a component of a machine, be correctly installed.
"EMI Source-Victim Model" shows the commonly used EMI model. The model consists of an EMI source, a coupling mechanism and an EMI victim. A device such as servo drives and computers, which contain switching power supplies and microprocessors, are EMI sources. The mechanisms for the coupling of energy between the source and victim are conduction and radiation. Victim equipment can be any electromagnetic device that is adversely affected by the EMI coupled to it.


Figure I.1- EMI Source-Victim Model

Immunity to EMI is primarily determined by equipment design, but how you wire and ground the device is also critical to achieving EMI immunity. Therefore, it is important to select equipment that has been designed and tested for industrial environments. The EMI standards for industrial equipment include the EN61000-4-X series (IEC 1000-4-X and IEC8O1-X), EN55011 (CISPR11), ANSI C62 and C63 and

MIL-STD-461. Also, in industrial environments, you should use encoders with differential driver outputs rather than single ended outputs, and digital inputs/outputs with electrical isolation, such as those provided with optocouplers.

The EMI model provides only three options for eliminating the EMC problem:

- Reduce the EMI at the source
- Increase the victim's immunity to EMI (harden the victim)
- Reduce or eliminate the coupling mechanism

In the case of servo drives, reducing the EMI source requires slowing power semiconductor switching speeds. However, this adversely affects drive performance with respect to heat dissipation and speed/torque regulation. Hardening the victim equipment may not be possible, or practical. The final and often the most realistic solution is to reduce the coupling mechanism between the source and victim. Filtering, shielding and grounding can achieve this.

## Filtering

As mentioned above, high frequency energy can be coupled between circuits via radiation or conduction. The AC power wiring is one of the most important paths for both types of coupling mechanisms. The AC line can conduct noise into the drive from other devices, or it can conduct noise directly from the drive into other devices. It can also act as an antenna and transmit or receive radiated noise between the drive and other devices.

One method to improve the EMC characteristics of a drive is to use an isolation AC power transformer on the drive's input power. This minimizes inrush currents on power-up and provides electrical isolation. In addition, it provides common mode filtering, although the effect is limited in frequency by the inter-winding capacitance. Use of a Faraday shield between the windings can increase the common mode rejection bandwidth, (shield terminated to ground) or provide differential mode shielding (shield terminated to the winding). In some cases, an AC line filter will not be required unless other sensitive circuits are powered off the same AC branch circuit.
*Note: "Common mode" noise is present on all conductors that are referenced to ground. "Differential mode" noise is present on one conductor referenced to another conductor.

The use of properly matched AC line filters to reduce the conducted EMI emitting from the drive is essential in most cases. This allows nearby equipment to operate undisturbed. The basic operating principle is to minimize the high frequency power transfer through the filter. An effective filter achieves this by using capacitors and inductors to mismatch the source impedance (AC line) and the load impedance (drive) at high frequencies.

For drives brought for use in Europe, use of the correct filter is essential to meet emission requirements. Detailed information on filters is included in the manual and transformers should be used where specified in the manual.

## AC Line Filter Selection

Selection of the proper filter is only the first step in reducing conducted emissions. Correct filter installation is crucial to achieving both EMIL attenuation and to ensure safety. All of the following guidelines should be met for effective filter use.

1) The filter should be mounted to a grounded conductive surface.
2) The filter must be mounted close to the drive-input terminals, particularly with higher frequency missions ( $5-30 \mathrm{MHz}$ ). If the distance exceeds 600 mm (2 feet), a strap should be used to connect the drive and filter, rather than a wire.
3) The wires connecting the AC source to the filter should be shielded from, or at least separated from the wires (or strap) that connects the drive to the filter. If the connections are not segregated from each other, then the EMI on the drive side of the filter can couple over to the source side of the filter, thereby reducing, or eliminating the filter effectiveness. The coupling mechanism can be radiation, or stray capacitance between the wires. The best method of
achieving this is to mount the filter where the AC power enters the enclosure. "AC Line Filter Installation" shows a good installation and a poor installation.


Figure 2- AC Line Filter Installation
When multiple power cables enter A unfiltered line can contaminate a filtered line external to the enclosure. Therefore, all lines must be filtered to be effective. The situation is similar to a leaky boat. All the holes must be plugged to prevent sinking.

If the filter is mounted excessively far from the drive, it may be necessary to mount it to a grounded conductive surface, such as the enclosure, to establish a high frequency (HF) connection to that surface. To achieve the HF ground, direct contact between the mounting surface and the filter must be achieved. This may require removal of paint or other insulating material from the cabinet or panel.

## WARNING



Large leakage currents exist in AC line filters. They must be grounded properly before applying power. Filter capacitors retain high voltages after power removal. Before handling the equipment, voltages should be measured to determine safe levels prior to handling the equipment. Failure to observe this precaution could result in severe bodily injury.

The only reasonable filtering at the drive output terminals is the use of inductance. Capacitors would slow the output switching and deteriorate the drive performance. A common mode choke can be used to reduce the HF voltage at the drive output. This will reduce emission coupling through the drive back to the AC line. However, the motor cable still carries a large HF voltage and current. Therefore, it is very important to segregate the motor cable from the AC power cable. More information on cable shielding and segregation is contained in the section on shielding.

## Grounding

High frequency (HF) grounding is different from safety grounding. A long wire is sufficient for a safety ground, but is completely ineffective as a HF ground due to the wire inductance. As a rule of thumb, a wire has an inductance of $8 \mathrm{nH} / \mathrm{in}$ regardless of diameter. At low frequencies, it acts as constant impedance, at intermediate frequencies as an inductor, and at high frequencies as an antenna. The use of ground straps is a better alternative to wires. However, the length to width ratio must be 5:1, or better yet 3:1, to remain a good high frequency connection.

The ground system's primary purpose is to function as a return current path. It is commonly thought of as an equipotential circuit reference point, but different locations in a ground system may be at different potentials. This is due to the return current flowing through the ground systems finite impedance. In a sense, ground systems are the sewer systems of electronics and as such
are sometimes neglected.
The primary objective of a high frequency ground system is to provide a well-defined path for HF currents and to minimize the loop area of the HF current paths. It is also important to separate HF grounds from sensitive circuit grounds. "Single Point Ground Types" shows single point grounds for both series (daisy chain) and parallel (separate) connections. A single point, parallel connected ground system is recommended.


## GROUND BUS BAR

Figure 3-Single Point Ground Types
A ground bus bar or plane should be used as the "single point" where circuits are grounded. This will minimize common (ground) impedance noise coupling. The ground bus bar (GBB) should be connected to the AC ground, and if necessary, to the enclosure. All circuits or subsystems should be connected to the GBB by separate connections. These connections should be as short as possible and straps should be used when possible. The motor ground conductor must return to the ground terminal on the drive, not the GBB.

## Shielding and Segregation

The EMI radiating from the drive enclosure drops off very quickly over distance. Mounting the drive in an enclosure, such as an industrial cabinet, further reduces the radiated emissions. The cabinet should have a high frequency ground and the size of the openings should be minimized. In addition, the drive is considered an "open" device that does not provide the proper IP rating for the environment in which it is installed. For this reason, the enclosure must provide the necessary degree of protection. An IP rating or Nema rating (which is similar to IP) specifies the degree of protection that an enclosure provides.

The primary propagation route for EMI emissions from a drive is through cabling. The cables conduct the EMI to other devices, and can also radiate the EMI. For this reason, cable segregation and shielding are important factors in reducing emissions. Cable shielding can also increase the level of immunity for a drive.

## For example:

- Shield termination at both ends is extremely important. The common misconception that shields should be terminated at only one end originates from audio applications with frequencies <20 kHz. RF applications must be terminated with the shield at both ends, and possibly at intermediate points for exceptionally long cables.
- When shielded cables are not terminated at the cable connection and pass through the wall of a cabinet, the shield must be bonded to the cabinet wall to prevent noise acquired inside the cabinet from radiating outside the cabinet, and vice versa.
- When shielded cables are terminated to connectors, the shield must be able to provide complete $360^{\circ}$ coverage and terminate through the connector backshell. The shield must not be grounded inside the connector through a drain wire. Grounding the shield inside the connector couples the noise on the shield to the signal conductors sharing the connector and virtually guarantees failure to meet European EMC requirements.
- The shield must be continuous. Each intermediate connector must continue the shield connection through the backshell.
- All cables, both power and signal should use twisted wire pairing.

The shield termination described above provides a coaxial type of configuration, which provides magnetic shielding, and the shield provides a return path for HF currents that are capacitive coupled from the motor windings to the frame. If power frequency circulating currents are an issue, a 250 VAC capacitor should be used at one of the connections to block $50 / 60 \mathrm{~Hz}$ current while passing HF currents. Use of a properly shielded motor cable is essential to meet European EMC requirements.

The following suggestions are recommended for all installations.

1. Motor cables must have a continuous shield and be terminated at both ends. The shield must connect to the ground bus bar or drive chassis at the drive end, and the motor frame at the motor end. Use of a properly shielded motor cable is essential to meet European EMC requirements.
2. Signal cables (encoder, serial, and analog) should be routed away from the motor cable and power wiring. Separate steel conduit can be used to provide shielding between the signal and power wiring. Do not route signal and power wiring through common junctions or raceways.
3. Signal cables from other circuits should not pass within $300 \mathrm{~mm}(1 \mathrm{ft}$ ) of the drive.
4. The length or parallel runs between other circuit cables and the motor or power cable should be minimized. A rule of thumb is $300 \mathrm{~mm}(1 \mathrm{ft}$.) of separation for each $10 \mathrm{~m}(30 \mathrm{ft}$.) of parallel run. The $300 \mathrm{~mm}(1 \mathrm{ft}$.$) separation can be reduced if the parallel run is less than 1 \mathrm{~m}(3 \mathrm{ft}$.).
5. Cable intersections should always occur at right angles to minimize magnetic coupling.
6. The encoder mounted on the brushless servomotor should be connected to the drive with a cable using multiple twisted wire pairs and an overall cable shield. Encoder cables are offered in various lengths that have correct terminations.

Persistent EMI problems may require additional countermeasures. The following suggestions for system modification may be attempted.

1. A ferrite toroid or "doughnut" around a signal cable may attenuate common mode noise, particularly RS-232 communication problems. However, a ferrite toroid will not help differential mode noise. Differential mode noise requires twisted wire pairs.
2. Suppress each switched inductive device near the servo drive. Switch inductive devices include solenoids, relay coils, starter coils and AC motors (such as motor driven mechanical timers).
3. DC coils should be suppressed with a "free-wheeling" diode connected across the coil.
4. AC coils should be suppressed with RC filters (a 200 Ohm $1 / 2$ Watt resistor in series with a 0.5 $\mu \mathrm{F}, 600$ Volt capacitor is common).

Following these guidelines can minimize noise problems. However, equipment EMC performance must meet regulatory requirements in various parts of the world, specifically the European Union. Ultimately, it is the responsibility of the machine builder to ensure that the machine meets the appropriate requirements as installed.

## Declaration of Incorporation Motion Control Systems



The undersigned hereby declares that the equipment specified above conforms to the noted Directives and Standards.

## MANUFACTURER

## 

HELEN M. VASAK
SECRETARY-TREASURER
6-1-2021
$\begin{array}{ll}\text { Prepared By: } & \text { Intertek Testing Services, Laguna Niguel, CA } \\ \text { Confirmed By: } & \text { John Quigley, Quality Manager }\end{array}$

## Digital PWM Brushless Servo Drives

- PWM (Pulse-Width-Modulated) Brushless servo Drives to 20KW


## Analog Brush Type Servo Drives

- Linear Brush type servo Drives to 2.6KW
- PWM (Pulse-Width-Modulated) Brush type servo Drives to 28KW


## Analog Brushless Servo Drives

- Linear Brushless servo Drives to 3.5KW
- PWM (Pulse-Width-Modulated) Brushless servo Drives to 51 KW


## Permanent Magnet DC Brush Type Servo Motors

- Continuous Torques to 335 in . Ib.
- Peak Torques to 2100 in . lb.


## Permanent Magnet DC Brushless Servo Motors

- Continuous Torques to 1100 in . lb.
- Peak Torques to 2200 in. lb.

